

### Example 1 – Investigation of a Slender Nonway Column

Determine the adequacy of a 4" x 20" column<sup>1</sup> with 3-#11 bars on each 14" side in a nonway frame with a clear height of 22'6". Use  $k=1.0$ .

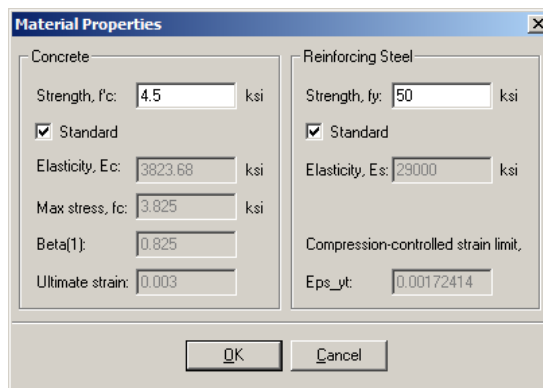
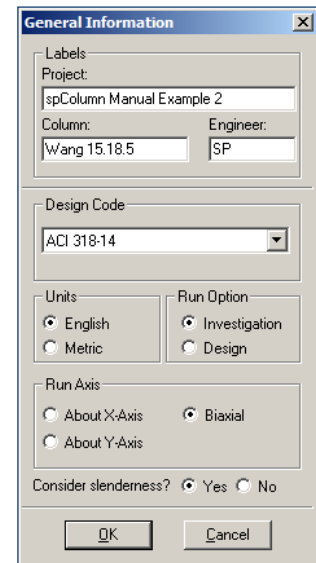
The concrete used is 6000 psi and the reinforcing steel is 60,000 psi.

The factored load values for the column under consideration are as follows:

$P$ (kip)	115 kips
Top $M_{uy}$ (kip-ft)	279 ft-kips
Bottom $M_{uy}$ (kip-ft)	-279 ft-kips

From the **File** menu, choose **New**. Any input data is cleared and the default values are restored.

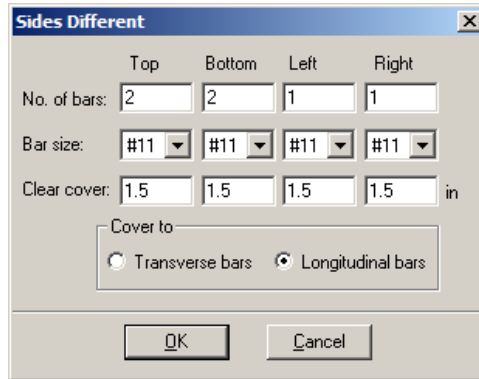
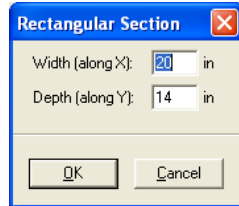
- From the **Input** menu, choose **General Information**.
  - Input the PROJECT header.
  - Select ENGLISH units and ACI 318-14 code.
  - Select Biaxial for run axis, Investigation for run option and Yes for Consider Slenderness?
  - Choose OK.
- From the **Input** menu, choose **Material Properties**.
  - Input 4.5 for the CONCRETE STRENGTH. Change the REINFORCING STEEL STRENGTH to 50. Other properties are computed and will be accepted.
  - Choose Ok.



From the **Input** menu, choose **Section | Rectangular**.

- Input 20 and 14 for the section width (along X) and depth (along Y).
- Choose OK.

<sup>1</sup> Based on Example 15.8.5 from Reinforced Concrete Design by Chu-Kia Wang, Charles G. Salmon, and Jose A. Pincheira, Seventh Edition, 2007, John Wiley and Sons, Inc.

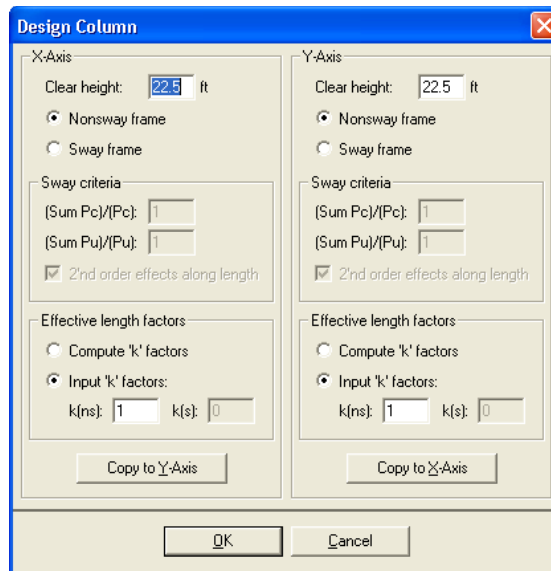


3. From the **Input** menu, choose **Reinforcement | Sides Different**.

- Input 2-#11 bars for TOP and BOTTOM and 1-#11 for LEFT and RIGHT. Input 1.5 in for the cover and select LONGITUDINAL BARS.
- Choose OK.

4. From the **Input** menu, choose **Slenderness | Design Column**.

- Input 22.5 for the column CLEAR HEIGHT.
- Check NONSWAY FRAME and select INPUT 'K' FACTORS.
- Choose OK.



5. From the **Input** menu, choose **Loads | Service**.

- Under LIVE, input 71.875 for the AXIAL LOAD, 0 for the X-MOMENTS @TOP, 0 for the X-MOMENTS @BOT, 174.375 for the Y-MOMENTS @TOP and -174.375 for the Y-MOMENTS @BOTTOM, respectively.
- In column SUSTAINED LOAD keep default setting for dead load equal 100%.
- Choose INSERT to add the entry to the list box.
- Choose OK .

	Axial Load (kip)	X-Moments (k-ft)		Y-Moments (k-ft)		Sustained Load (%)
		@ Top	@ Bot	@ Top	@ Bot	
Dead:	0	0	0	0	0	100
Live:	71.875	0	0	174.375	-174.375	0
Wind:	0	0	0	0	0	0
EQ:	0	0	0	0	0	0
Snow:	0	0	0	0	0	0

No. [P, Mxt, Mxb, Myt, Myb] for each case

1	D	[0.0, 0.0, 0.0]	L	[71.875, 0.0, 174.375, -174.375]	W	[0.0, 0.0, 0.0, 0.0]	E	[0.0, 0.0, 0.0, 0.0]	S	[0.0, 0.0, 0.0]
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6. From the **Input** menu, choose **Loads | Load Combinations**.

- If the list displays thirteen combinations, choose only the second load combination U2 and delete all the others by selecting them and using DELETE. Choose OK.

	Dead	Live	Wind	EQ	Snow
	1.2	1.6	0	0	0.5

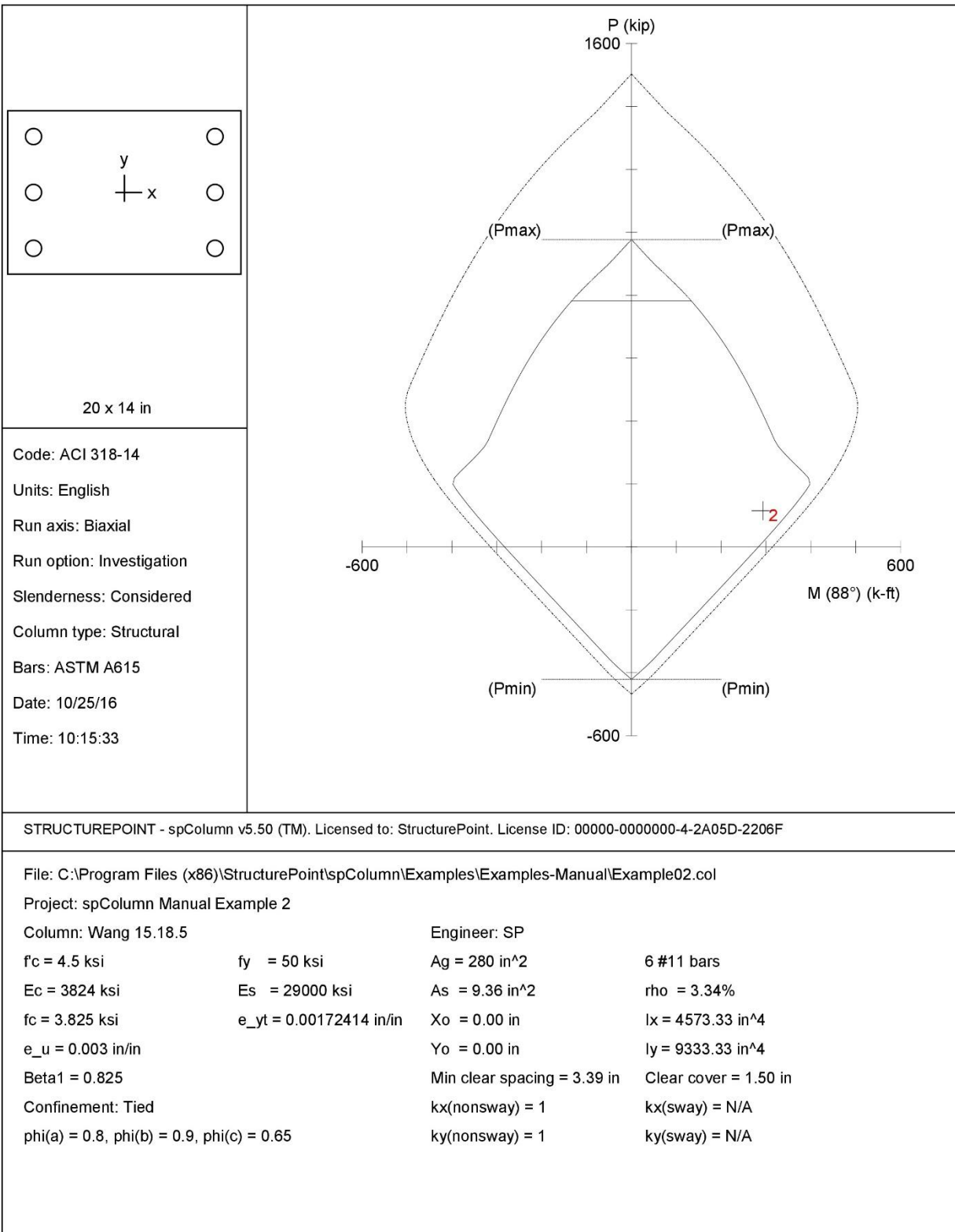
Combo	Dead	Live	Wind	EQ	Snow
U1	1.2	1.6	0	0	0.5

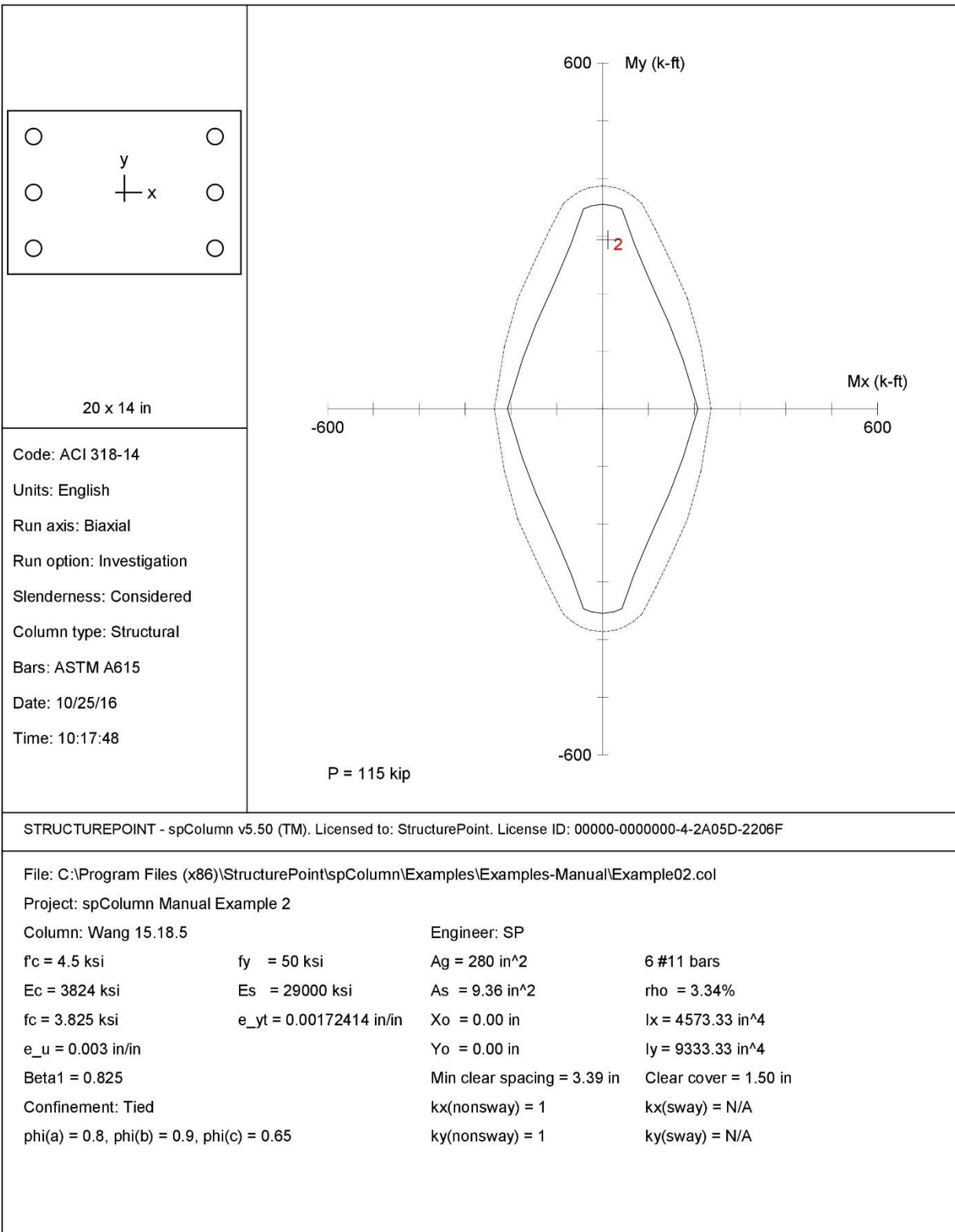
7. From the **Solve** menu, choose **Execute**.

- The solver of the program is started and, upon completion, displays the interaction diagram of the section with the load point plotted within the diagram.

8. From the **View** menu, choose **Results**.

- 
- Page through the results file.
  - Choose FILE | EXIT to quit the spView program and get back to spColumn.
9. From the **File** menu, choose **Print Results**.
- Select the printer to send the text results to.
  - Choose PRINT.
10. From the **File** menu, choose **Print Screen**.
- Select the printer to send the graphical results to.
  - Choose PRINT.





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 C:\Program Files (x86)\StructurePoint\spColumn\Examples\Examples-Manual\Example02.col

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General Information:

=====  
 File Name: C:\Program Files (x86)\StructurePoint\spColumn\Examples\Examples-Manual\Example02.col  
 Project: spColumn Manual Example 2  
 Column: Wang 15.18.5                      Engineer: SP  
 Code: ACI 318-14                              Units: English  
  
 Run Option: Investigation                      Slenderness: Considered  
 Run Axis: Biaxial                              Column Type: Structural

Material Properties:

=====  
 Concrete: Standard                              Steel: Standard  
 f'c = 4.5 ksi                                      fy = 50 ksi  
 Ec = 3823.68 ksi                                  Es = 29000 ksi  
 fc = 3.825 ksi                                    Eps\_yt = 0.00172414 in/in  
 Eps\_u = 0.003 in/in  
 Beta1 = 0.825

Section:

=====  
 Rectangular: Width = 20 in                      Depth = 14 in  
  
 Gross section area, Ag = 280 in^2  
 Ix = 4573.33 in^4                                  Iy = 9333.33 in^4  
 rx = 4.04145 in                                   ry = 5.7735 in  
 Xo = 0 in    Yo = 0 in

Reinforcement:

=====  
 Bar Set: ASTM A615  

Size	Diam (in)	Area (in^2)	Size	Diam (in)	Area (in^2)	Size	Diam (in)	Area (in^2)
# 3	0.38	0.11	# 4	0.50	0.20	# 5	0.63	0.31
# 6	0.75	0.44	# 7	0.88	0.60	# 8	1.00	0.79
# 9	1.13	1.00	# 10	1.27	1.27	# 11	1.41	1.56
# 14	1.69	2.25	# 18	2.26	4.00			

Confinement: Tied; #3 ties with #11 bars, #4 with larger bars.  
 phi(a) = 0.8, phi(b) = 0.9, phi(c) = 0.65

Layout: Rectangular  
 Pattern: Sides Different (Cover to longitudinal reinforcement)  
 Total steel area: As = 9.36 in^2 at rho = 3.34%  
 Minimum clear spacing = 3.39 in

	Top	Bottom	Left	Right
Bars	2 #11	2 #11	1 #11	1 #11
Cover(in)	1.5	1.5	1.5	1.5

Service Loads:

No. Case	Load	Axial Load kip	Mx @ Top k-ft	Mx @ Bot k-ft	My @ Top k-ft	My @ Bot k-ft
1	Dead	0.00	0.00	0.00	0.00	0.00
	Live	71.88	0.00	0.00	174.38	-174.38
	Wind	0.00	0.00	0.00	0.00	0.00
	EQ	0.00	0.00	0.00	0.00	0.00
	Snow	0.00	0.00	0.00	0.00	0.00

Sustained Load Factors:

Load Case	Factor (%)
Dead	100
Live	0
Wind	0
EQ	0
Snow	0

Load Combinations:

=====  
 U1 = 1.200\*Dead + 1.600\*Live + 0.000\*Wind + 0.000\*Earthquake + 0.500\*Snow

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Slenderness:

Sway Criteria:

X-axis: Nonsway column.  
Y-axis: Nonsway column.

Column	Axis	Height ft	Width in	Depth in	I in <sup>4</sup>	f'c ksi	Ec ksi
Design	X	22.5	20	14	4573.33	4.5	3823.68
	Y	22.5	20	14	9333.33	4.5	3823.68
Above	X	(no column specified...)					
	Y	(no column specified...)					
Below	X	(no column specified...)					
	Y	(no column specified...)					

X-Beams Location	Length ft	Width in	Depth in	I in <sup>4</sup>	f'c ksi	Ec ksi
Above Left	(no beam specified...)					
Above Right	(no beam specified...)					
Below Left	(no beam specified...)					
Below Right	(no beam specified...)					

Y-Beams Location	Length ft	Width in	Depth in	I in <sup>4</sup>	f'c ksi	Ec ksi
Above Left	(no beam specified...)					
Above Right	(no beam specified...)					
Below Left	(no beam specified...)					
Below Right	(no beam specified...)					

Effective Length Factors:

Axis	Psi (top)	Psi (bot)	k(Nonsway)	k(Sway)	klu/r
X	0.000	0.000	1.000	(N/A)	66.81
Y	0.000	0.000	1.000	(N/A)	46.77

Moment Magnification Factors:

Stiffness reduction factor, phi(K) = 0.75  
Cracked-section coefficients: cI(beams) = 0.35; cI(columns) = 0.7

0.2\*Ec\*Ig + Es\*Ise (X-axis) = 7.66e+006 kip-in<sup>2</sup>  
0.2\*Ec\*Ig + Es\*Ise (Y-axis) = 2.36e+007 kip-in<sup>2</sup>

X-axis		At Ends					Along Length				
Ld/Comb	SumPu (kip)	Pc (kip)	SumPc (kip)	Betads	Deltas	Pu (kip)	k'lu/r	Pc (kip)	Betad	Cm	Delta
1 U1	(N/A)	(N/A)	(N/A)	(N/A)	(N/A)	115.00	(N/A)	1036.79	0.000	1.000	1.174

Y-axis		At Ends					Along Length				
Ld/Comb	SumPu (kip)	Pc (kip)	SumPc (kip)	Betads	Deltas	Pu (kip)	k'lu/r	Pc (kip)	Betad	Cm	Delta
1 U1	(N/A)	(N/A)	(N/A)	(N/A)	(N/A)	115.00	(N/A)	3199.27	0.000	1.000	1.050

Factored Moments due to First-Order and Second-Order Effects:

Minimum eccentricity, Ex,min = 1.02 in  
Minimum eccentricity, Ey,min = 1.2 in

NOTE: Each loading combination includes the following cases:  
First line - at column top  
Second line - at column bottom

X-axis		1st Order			2nd Order			Ratio
Load	Mns k-ft	Ms k-ft	Mu k-ft	Mmin k-ft	Mi k-ft	Mc k-ft	2nd/1st	
1 U1	0.00	(N/A)	0.00	9.78	M1= 0.00	11.47	1.174	
	-0.00	(N/A)	-0.00	9.78	M2= -0.00	11.47	1.174	
Y-axis		1st Order			2nd Order			Ratio
Load	Mns k-ft	Ms k-ft	Mu k-ft	Mmin k-ft	Mi k-ft	Mc k-ft	2nd/1st	
1 U1	279.00	(N/A)	279.00	11.50	M1= 279.00	293.04	1.050	
	279.00	(N/A)	279.00	11.50	M2= 279.00	293.04	1.050	



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Factored Loads and Moments with Corresponding Capacities:

NOTE: Each loading combination includes the following cases:

First line - at column top

Second line - at column bottom

No.	Load Combo	Pu kip	Mux k-ft	Muy k-ft	PhiMnx k-ft	PhiMny k-ft	PhiMn/Mu	NA depth in	Dt depth in	eps_t	Phi
1	1 U1	115.00	11.47	293.04	13.83	353.32	1.206	5.19	18.77	0.00810	0.900
2		115.00	11.47	293.04	13.83	353.32	1.206	5.19	18.77	0.00810	0.900

\*\*\* End of output \*\*\*

## Example 2 – Design of a Slender Column in a Sway Frame

Design a square column<sup>2</sup> with a clear height of 16 ft. The column is sway and subjected to dead, live and wind loads as shown below.

	<u>Dead</u>	<u>Live</u>	<u>Wind</u>
$P$ (kip)	380	140	0
Top $M_x$ (kip-ft)	32	20	50
Bottom $M_x$ (kip-ft)	54	36	50

The column is to be checked for the following load combinations:

$$U1 = 1.2 D + 1.6 L$$

$$U2 = 1.2 D + 0.5 L + 1.6 W$$

The calculations in the reference are done based on the load combination U2.

In practice, the ratio  $\Sigma P_c / P_c$  would have to be calculated before the problem can be attempted, using a trial value of  $\Sigma P_c / P_c$ . Here, the value of  $\Sigma P_c / P_c$  used is 28.67 based on the reference value of  $P_c$ . There are 14 interior columns, 18 exterior columns and 4 corner columns. Therefore, the value of  $\Sigma P_u / P_u = 14 + 18 * 2/3 + 4 * 1/3 = 27.33$  irrespective of the load combination being used.

- From the **File** menu, choose **New**. Any input data is cleared and the default values are restored.
- From the **Input** menu, choose **General Information**.
  - Input the PROJECT header.
  - Select English units and ACI 318-14 code.
  - Select About X-Axis for run axis, Design for run option and Yes for Consider slenderness?
  - Choose OK.
- From the **Input** menu, pick **Material Properties**.
  - Input 5 for the concrete strength. Other properties are computed and will be accepted.
  - Choose OK.

<sup>2</sup> Based on Example 12.4, pp 409, from Structural Concrete: Theory and Design by M. Nadim Hassoun and Akthem Al-Manaseer, Fourth Edition, 2008, John Wiley and Sons, Inc.

The dialog box is titled "Material Properties" and is divided into two main sections: "Concrete" and "Reinforcing Steel".

**Concrete Section:**

- Strength,  $f_c$ : 5 ksi
- Standard
- Elasticity,  $E_c$ : 4030.51 ksi
- Max stress,  $f_c$ : 4.25 ksi
- Beta(1): 0.8
- Ultimate strain: 0.003

**Reinforcing Steel Section:**

- Strength,  $f_y$ : 60 ksi
- Standard
- Elasticity,  $E_s$ : 29000 ksi
- Compression-controlled strain limit,  $E_{ps\_yt}$ : 0.00206897

Buttons: OK, Cancel

4. From the **Input** menu, pick **Section | Rectangular**.

- Input 18 and 18 for the WIDTH (ALONG X) and DEPTH (ALONG Y) under both START and END options.
- Choose OK.

The dialog box is titled "Rectangular Section" and contains a table for defining dimensions.

	Start	End	Increment
Width (along X):	18	18	0 in
Depth (along Y):	18	18	0 in

Buttons: OK, Cancel

5. From the **Input** menu, choose **Reinforcement | All Sides Equal**

- Input 4-#10 bars for Minimum, and 40-#10 bars for Maximum and 1.5 in for the cover, and select TRANSVERSE BARS and RECTANGULAR Bar Layout.
- Choose OK.

The dialog box is titled "All Sides Equal" and contains the following settings:

- Minimum No. of bars: 4
- Maximum No. of bars: 40
- Bar size: #10 (selected)
- Clear cover: 1.5 in
- Cover to:  Transverse bars,  Longitudinal bars
- Bar Layout:  Rectangular,  Circular

Buttons: OK, Cancel

6. From the **Input** menu, choose **Slenderness | Design Column**.

- Input 16 for the column CLEAR HEIGHT.
- Check SWAY FRAME
- Under SWAY CRITERIA, input 28.67 and 27.33 for the  $\Sigma P_c/P_c$  and  $\Sigma P_u/P_u$ , respectively.
- Leave 2<sup>ND</sup> ORDER EFFECT ALONG LENGTH option checked (default)
- Select COMPUTE 'K' FACTORS.
- Choose OK.

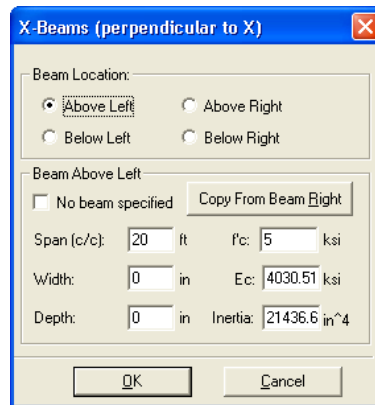
7. From the **Input** menu, choose **Slenderness | Columns Above/Below**.

- Clear the NO COLUMN SPECIFIED option.
- Input 11 for the column height (center-to-center) under HEIGHT (C/C) and leave the other data as is.
- Choose Copy to Column Below.
- Choose OK.

8. From the **Input** menu, choose **Slenderness | X-Beams**.

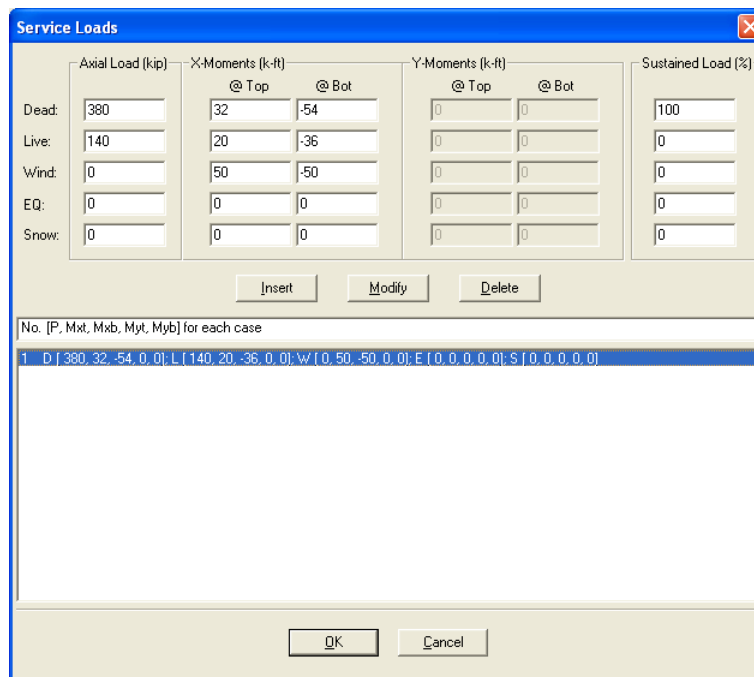
- Choose ABOVE LEFT.
- Clear the NO BEAM SPECIFIED option.
- Input 20 for the span (center-to-center) under SPAN(C/C).
- Input 0.00 and 0.00 for the WIDTH and DEPTH, respectively.
- Input 21436.6 for the moment of inertia under INERTIA.
- Leave the other data as it is.
- Choose ABOVE RIGHT and click on COPY FROM BEAM LEFT.
- Choose BELOW LEFT and click on COPY FROM BEAM ABOVE.

- Choose **BELOW RIGHT** and click on **COPY FROM BEAM ABOVE**.
- Choose **OK**.



9. From the **Input** menu, choose **Loads | Service**.

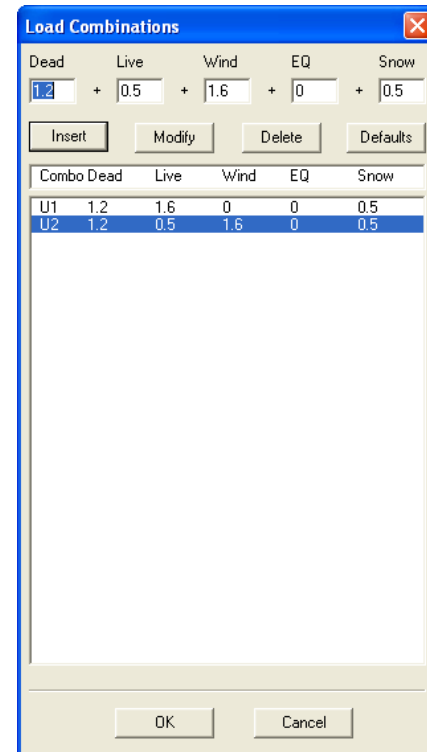
- Under **DEAD**, input 380, 32 and -54 for the **AXIAL LOAD**, **X-MOMENTS** and **Y-MOMENTS** respectively.
- Under **LIVE**, input 140, 20 and -36 for the **AXIAL LOAD**, **X-MOMENTS** and **Y-MOMENTS**, respectively.
- Under **WIND**, input 0, 50 and -50 for the **AXIAL LOAD**, **X-MOMENTS** and **Y-MOMENTS**, respectively.

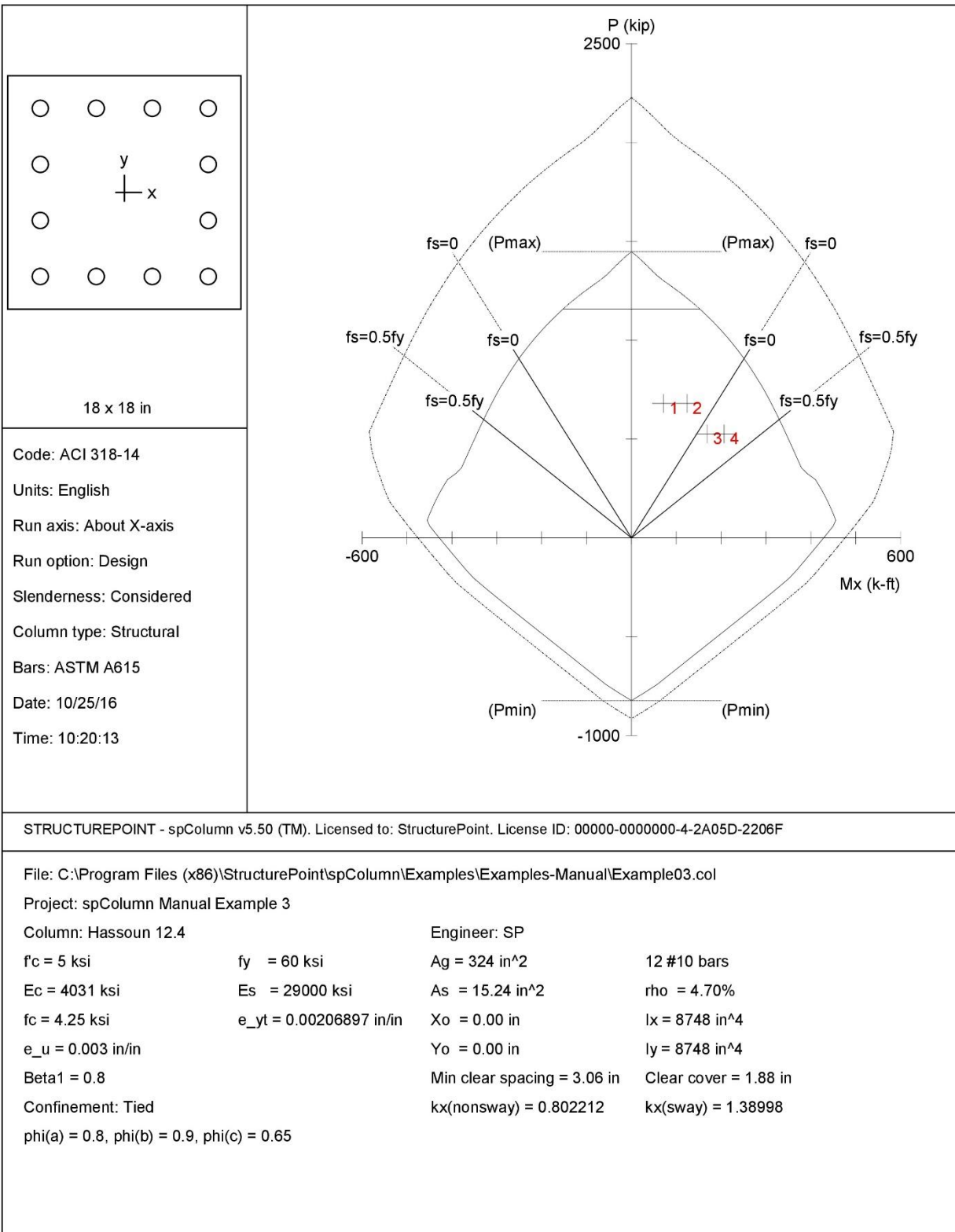


- Under **SUSTAINED LOAD** keep the default settings of 100% for dead and 0% for all other load cases.
- Choose **INSERT** to add the entry to the list box.
- Choose **OK**.

10. From the **Input** menu, choose **Loads | Load Combinations**.

- If the list displays thirteen combinations, leave the first and second as they are. Delete the remaining combinations using DELETE.
11. From the **Solve** menu, choose **Execute**.
    - The solver of the program is started and, upon completion, displays the interaction diagram of the section with the load points plotted within the diagram.
  12. From the **View** menu, choose **Results**.
    - Page through the results file.
    - Choose Exit to quit the spView program and get back to spColumn.
  13. From the **File** menu, choose **Print Results**.
    - Select the printer to send the text results to.
    - Choose PRINT.
  14. From the **File** menu, choose **Print Screen**.
    - Select the printer to send the graphical results to.
    - Choose PRINT.





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General Information:

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=====
File Name: C:\Program Files (x86)\StructurePoint\spColumn\Examples\Examples-Manual\Example03.col
Project:  spColumn Manual Example 3
Column:  Hassoun 12.4                Engineer: SP
Code:    ACI 318-14                 Units: English

Run Option: Design                    Slenderness: Considered
Run Axis:  X-axis                     Column Type: Structural
    
```

Material Properties:

```

=====
Concrete: Standard                    Steel: Standard
f'c = 5 ksi                          fy = 60 ksi
Ec = 4030.51 ksi                     Es = 29000 ksi
fc = 4.25 ksi                        Eps_yt = 0.00206897 in/in
Eps_u = 0.003 in/in
Beta1 = 0.8
    
```

Section:

```

=====
Rectangular: Width = 18 in           Depth = 18 in

Gross section area, Ag = 324 in^2
Ix = 8748 in^4                      Iy = 8748 in^4
rx = 5.19615 in                     ry = 5.19615 in
Xo = 0 in                            Yo = 0 in
    
```

Reinforcement:

```

=====
Bar Set: ASTM A615
Size Diam (in) Area (in^2)  Size Diam (in) Area (in^2)  Size Diam (in) Area (in^2)
-----
# 3      0.38      0.11  # 4      0.50      0.20  # 5      0.63      0.31
# 6      0.75      0.44  # 7      0.88      0.60  # 8      1.00      0.79
# 9      1.13      1.00  # 10     1.27      1.27  # 11     1.41      1.56
# 14     1.69      2.25  # 18     2.26      4.00
    
```

Bar selection: Minimum number of bars  
Asmin = 0.01 \* Ag = 3.24 in^2, Asmax = 0.08 \* Ag = 25.92 in^2

Confinement: Tied; #3 ties with #10 bars, #4 with larger bars.  
phi(a) = 0.8, phi(b) = 0.9, phi(c) = 0.65

Layout: Rectangular  
Pattern: All Sides Equal (Cover to transverse reinforcement)  
Total steel area: As = 15.24 in^2 at rho = 4.70%  
Minimum clear spacing = 3.06 in

12 #10 Cover = 1.5 in

Service Loads:

```

=====
Load   Axial Load   Mx @ Top   Mx @ Bot   My @ Top   My @ Bot
No. Case  kip          k-ft       k-ft       k-ft       k-ft
-----
1 Dead   380.00       32.00      -54.00     0.00       0.00
  Live  140.00       20.00      -36.00     0.00       0.00
  Wind   0.00         50.00      -50.00     0.00       0.00
  EQ     0.00         0.00       0.00       0.00       0.00
  Snow   0.00         0.00       0.00       0.00       0.00
    
```

Sustained Load Factors:

```

=====
Load   Factor
Case   (%)
-----
Dead   100
Live   0
Wind   0
EQ     0
Snow   0
    
```

Load Combinations:

```

=====
U1 = 1.200*Dead + 1.600*Live + 0.000*Wind + 0.000*Earthquake + 0.500*Snow
U2 = 1.200*Dead + 0.500*Live + 1.600*Wind + 0.000*Earthquake + 0.500*Snow
    
```



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Slenderness:

Sway Criteria:

X-axis: Sway column. SumPc = 28.67 \* Pc SumPu = 27.33 \* Pu  
 Second-order effects along length considered

Column Axis	Height ft	Width in	Depth in	I in <sup>4</sup>	f'c ksi	Ec ksi
Design X	16	18	18	8748	5	4030.51
Above X	11	18	18	8748	5	4030.51
Below X	11	18	18	8748	5	4030.51

X-Beams Location	Length ft	Width in	Depth in	I in <sup>4</sup>	f'c ksi	Ec ksi
Above Left	20	0	0	21436.6	5	4030.51
Above Right	20	0.0001	0.0001	21436.6	5	4030.51
Below Left	20	0.0001	0.0001	21436.6	5	4030.51
Below Right	20	0.0001	0.0001	21436.6	5	4030.51

Effective Length Factors:

Axis	Psi(top)	Psi(bot)	k(Nonsway)	k(Sway)	klu/r
X	1.252	1.252	0.802	1.390	51.36

Moment Magnification Factors:

Stiffness reduction factor, phi(K) = 0.75  
 Cracked-section coefficients: cI(beams) = 0.35; cI(columns) = 0.7

$0.2 * Ec * I_g + Es * I_{se} \text{ (X-axis)} = 2.02e+007 \text{ kip-in}^2$

X-axis Ld/Comb	At Ends					Along Length					
	SumPu(kip)	Pc(kip)	SumPc(kip)	Betads	Deltas	Pu(kip)	k'lu/r	Pc(kip)	Betad	Cm	Delta
1 U1	18584.40	2792.45	80059.54	0.000	1.448	680.00	(N/A)	5018.30	0.671	0.830	1.013
U2	14375.58	2792.45	80059.54	0.000	1.315	526.00	(N/A)	4490.56	0.867	0.927	1.098

Factored Moments due to First-Order and Second-Order Effects:

Minimum eccentricity, Ex,min = 1.14 in

NOTE: Each loading combination includes the following cases:  
 First line - at column top  
 Second line - at column bottom

X-axis Load Combo	1st Order				2nd Order			Ratio 2nd/1st
	Mns k-ft	Ms k-ft	Mu k-ft	Mmin k-ft	Mi k-ft	Mc k-ft		
1 U1	70.40	0.00	70.40	64.60	M1= 70.40	71.32	1.013	
	122.40	-0.00	122.40	64.60	M2= 122.40	124.00	1.013	
1 U2	48.40	80.00	128.40	49.97	M1= 153.58	168.69	1.314	
	82.80	80.00	162.80	49.97	M2= 187.98	206.47	1.268	

Factored Loads and Moments with Corresponding Capacities:

Design/Required ratio PhiMn/Mu >= 1.00

NOTE: Each loading combination includes the following cases:  
 First line - at column top  
 Second line - at column bottom

No.	Load Combo	Pu kip	Mux k-ft	PhiMnx k-ft	PhiMn/Mu	NA depth in	Dt depth in	eps_t	Phi
1	1 U1	680.00	71.32	311.55	4.368	12.43	15.49	0.00074	0.650
2		680.00	124.00	311.55	2.512	12.43	15.49	0.00074	0.650
3	1 U2	526.00	168.69	344.47	2.042	10.76	15.49	0.00132	0.650
4		526.00	206.47	344.47	1.668	10.76	15.49	0.00132	0.650

\*\*\* End of output \*\*\*